

# Some theorems in Luikov's theory of heat and mass transfer in capillary-porous bodies

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(Received 2 October 1987)

**Abstract**—The linear theory of heat and mass transfer is considered. Some general theorems are formulated, i.e. a reciprocity theorem and a variational theorem (no use is made of the Laplace transform). The functional derived herein gives all the governing equations, including the boundary and initial conditions, as Euler equations.

## INTRODUCTION

THE INTERRELATION between heat and mass transfer in porous bodies was first established by Luikov [1, 2] who proposed a two-term relationship for non-isothermal mass diffusion and also determined experimentally the coefficients of diffusion and thermo-diffusion for a number of moist materials. Later [3, 4] via the use of thermodynamics of irreversible processes, he defined a coupled system of partial differential equations for heat and mass transfer potential distributions in porous bodies. Applications in this and other fields such as drying theory, building thermo-physics and heat and moisture migration in soils can be found in ref. [5]. Independently, Krischer [6] and De Vries [7] also proposed systems of differential equations of the Luikov type for temperature and moisture content distributions in porous bodies.

The analytical solution of these types of equations presents great mathematical difficulties, and consequently solutions are given for only the simplest of geometrical configurations and boundary conditions [4]. In any realistic problem resort must be made to numerical techniques. These have usually been based on some general theorems, i.e. a reciprocity theorem and a variational theorem.

The variational formulation based on local potential to simplified non-linear heat and mass transfer equations was proposed by Kumar [8]. Glazunov [9] proved that for the non-linear transport problem variational classic type theorems do not exist. Some non-classic type principles for solution of the non-linear interrelated heat and mass transfer problems are available in refs. [10-12].

In this paper Luikov's linear theory of heat and mass transfer is considered and the reciprocity theorem and the variational theorem are established. The procedure shown herein does not require any transformation of the field equations and includes the boundary and initial conditions.

## TRANSFER EQUATIONS

The governing equations in the linear theory of heat and mass transfer (Luikov's equations) are [3-5]

$$\frac{\partial T}{\partial t} = \left( a + \frac{\epsilon r a_m \delta}{c} \right) \Delta T + \frac{\epsilon r a_m}{c} \Delta W$$

$$\frac{\partial W}{\partial t} = a_m (\Delta W + \delta \Delta T), \quad x \in B, \quad t > 0 \quad (1)$$

where  $T$  denotes the temperature,  $W$  the mass content,  $a$  the thermal diffusivity,  $a_m$  the mass diffusivity,  $\epsilon$  the phase-change criterion (i.e.  $\epsilon = 1$  all vapour,  $\epsilon = 0$  all liquid),  $r$  the latent heat of evaporation,  $c$  the specific heat,  $\delta$  the thermogradient coefficient,  $x$  the spatial position,  $t$  the time, and  $\Delta$  the Laplace operator.

To the above field equations one adjoining the boundary conditions

$$q \equiv -\lambda \frac{\partial T}{\partial n} - \epsilon r a_m \rho \left( \frac{\partial W}{\partial n} + \delta \frac{\partial T}{\partial n} \right) = \hat{q}(x, t),$$

$$x \in \partial B_q, \quad t > 0 \quad (2)$$

$$j \equiv -a_m \rho \left( \frac{\partial W}{\partial n} + \delta \frac{\partial T}{\partial n} \right) = \hat{j}(x, t), \quad x \in \partial B_j, \quad t > 0 \quad (3)$$

$$T = \hat{T}(x, t), \quad x \in \partial B_T, \quad t > 0 \quad (4)$$

$$W = \hat{W}(x, t), \quad x \in \partial B_W, \quad t > 0 \quad (5)$$

and the initial conditions

$$T = T_0(x), \quad x \in \bar{B}, \quad t = 0 \quad (6)$$

$$W = W_0(x), \quad x \in \bar{B}, \quad t = 0 \quad (7)$$

where  $\lambda$  is the thermal conductivity,  $\rho$  the density of a perfectly dry body,  $\mathbf{n}$  the unit outward normal,  $\partial/\partial n$  the normal derivative;  $\hat{T}$  denotes the prescribed temperature on  $\partial B_T$ ,  $\hat{W}$  the moisture content on  $\partial B_W$ ,  $\hat{q}$

**NOMENCLATURE**

$a$	thermal diffusivity [ $m^2 s^{-1}$ ]	$\epsilon$	phase-change criterion
$a_m$	mass diffusivity [ $m^2 s^{-1}$ ]	$\lambda$	thermal conductivity [ $W m^{-1} K^{-1}$ ]
$A$	matrix operator	$\rho$	density [ $kg m^{-3}$ ].
$B$	body		
$\partial B$	boundary	<b>Subscripts and superscripts</b>	
$c$	specific heat [ $J kg^{-1} K^{-1}$ ]	$\alpha, \beta$	system
$E$	space	$\hat{\phantom{x}}$	surface
$f$	functional	$'$	dual
$\mathbf{f}$	vector	$0$	initial
$j$	mass flux [ $kg m^2 s^{-1}$ ]	$E$	space
$\mathbf{n}$	unit outward normal	$T, q$	heat
$q$	heat flux [ $W m^{-2}$ ]	$T$	transposition
$r$	heat of phase change [ $J kg^{-1}$ ]	$W, j$	mass.
$t$	time [s]		
$T$	temperature [K]	<b>Operators</b>	
$\mathbf{u}$	vector	$\nabla$	gradient
$W$	moisture content [ $kg kg^{-1}$ ]	$\Delta$	Laplacian
$x$	spatial position [m].	$*$	convolution
		$\cdot$	scalar product
<b>Greek symbols</b>		$\langle \cdot, \cdot \rangle$	bilinear form.
$\delta$	thermogradient coefficient [ $K^{-1}$ ]		

the heat flux on  $\partial B_q$ ,  $\hat{j}$  the mass flux on  $\partial B_j$ ;  $T_0$  and  $W_0$  are prescribed initial values;  $\bar{B} = B \cup \partial B$ .

The set of basic equations (1)–(7) can be put into the operator form

$$A\mathbf{u} + \mathbf{f} = \mathbf{0}, \quad A: E \rightarrow E', \mathbf{u} \in E, \mathbf{f} \in E' \quad (8)$$

where

$$\begin{aligned} \mathbf{u} &= [T, W; T, W; T, W, q, j]^T \quad (9) \\ \mathbf{f} &= [0, 0, -\delta c \rho T_0, -\epsilon r \rho W_0; \delta \hat{q}, \epsilon r \hat{j}, -\delta \hat{T}, -\epsilon r \hat{W}]^T \quad (10) \end{aligned}$$

and  $A$  is a linear matrix ( $8 \times 8$ ) operator the non-zero elements of which are given by

$$\begin{aligned} A_{11} &= \delta c \rho \left( \frac{\partial}{\partial t} - \left( a + \frac{\epsilon r a_m \delta}{c} \right) \Delta \right) \\ A_{12} &= -\epsilon r a_m \rho \Delta = A_{21} \\ A_{22} &= \epsilon r \rho \left( \frac{\partial}{\partial t} - a_m \Delta \right) \\ A_{33} &= \delta c \rho \\ A_{44} &= \epsilon r \rho \\ A_{57} &= -\delta = -A_{75} \\ A_{68} &= -\epsilon r = -A_{86}. \end{aligned} \quad (11)$$

Here  $E$  denotes the space of ordered arrays of the form given in equation (9). The dual space of  $E$  is denoted by  $E'$ .

**RECIPROCITY THEOREM**

Alternatively, one may consider a problem, equivalent to equation (8) given by [13]

$$\langle A\mathbf{u}, \mathbf{v} \rangle_E = \langle \mathbf{f}, \mathbf{v} \rangle_E, \quad \mathbf{v} \in E \quad (12)$$

where  $\langle \cdot, \cdot \rangle_E$  denotes the bilinear form on  $E \times E'$  represented by the integrals

$$\begin{aligned} \langle \mathbf{f}, \mathbf{v} \rangle_E &= \int_B (f_1 * v_1 + f_2 * v_2 + f_3(x, 0)v_3 \\ &+ f_4(x, 0)v_4) dV + \int_{\partial B_q} (f_5 * v_5) dS + \int_{\partial B_j} (f_6 * v_6) dS \\ &+ \int_{\partial B_T} (f_7 * v_7) dS + \int_{\partial B_W} (f_8 * v_8) dS \end{aligned} \quad (13)$$

where

$$\mathbf{f} = [f_1, \dots, f_8]^T, \quad \mathbf{v} = [v_1, \dots, v_8]^T.$$

In equation (13)  $f * v$  denotes the convolution of  $f$  and  $v$  [14]

$$f * v(x, t) = \int_0^t f(x, t - \tau)v(x, \tau) d\tau. \quad (14)$$

The capillary-porous body is considered subject to two different systems of heat and mass loadings  $\mathbf{f}^\alpha$  and two corresponding configurations  $\mathbf{u}^\alpha$ , where  $\alpha = 1, 2$ .

*Theorem 1.* If a capillary-porous body is subjected to two different systems of heat and mass loadings  $\mathbf{f}^\alpha$ , then between the corresponding configurations  $\mathbf{u}^\alpha$  there is the following relation:

$$\langle \mathbf{f}^1, \mathbf{u}^2 \rangle_E = \langle \mathbf{f}^2, \mathbf{u}^1 \rangle_E \quad (15)$$

where

$$\begin{aligned}
 \langle \mathbf{f}^\alpha, \mathbf{u}^\alpha \rangle_E = & \int_B (-\delta c \rho T^\alpha T_0^\beta - \epsilon r \rho W^\alpha W_0^\beta) dV \\
 & + \int_{\partial B_q} (\delta T^\alpha * \hat{q}^\beta) dS + \int_{\partial B_j} (\epsilon r W^\alpha * \hat{j}^\beta) dS \\
 & - \int_{\partial B_T} (\delta q^\alpha * \hat{T}^\beta) dS - \int_{\partial B_w} (\epsilon r j^\alpha * \hat{W}^\beta) dS, \\
 \alpha, \beta = & 1, 2, \alpha \neq \beta. \tag{16}
 \end{aligned}$$

*Proof.* On the basis of relation (12) one has

$$\langle \mathbf{A}\mathbf{u}^\alpha, \mathbf{u}^\beta \rangle_E = \langle \mathbf{f}^\alpha, \mathbf{u}^\beta \rangle_E, \quad \alpha, \beta = 1, 2, \alpha \neq \beta. \tag{17}$$

From equations (9)–(11), (13) and (17) (using Green's theorem and properties of the convolution), one obtains

$$\begin{aligned}
 \langle \mathbf{A}\mathbf{u}^1, \mathbf{u}^2 \rangle_E = & \rho \int_B \left( \delta c \left( \frac{\partial}{\partial t} (T^1 * T^2) \right. \right. \\
 & + \left. \left. \left( a + \frac{\epsilon r a_m \delta}{c} \right) \nabla T^1 * \nabla T^2 \right) + \epsilon r a_m \delta (\nabla T^1 * \nabla W^2 \right. \\
 & + \nabla W^1 * \nabla T^2) + \epsilon r \left( \frac{\partial}{\partial t} (W^1 * W^2) \right. \\
 & + \left. a_m \nabla W^1 * \nabla W^2 \right) \Big) dV + \int_{\partial B_T} (\delta (q^2 * T^1 \\
 & + q^1 * T^2)) dS + \int_{\partial B_w} (\epsilon r (j^2 * W^1 + j^1 * W^2)) dS
 \end{aligned} \tag{18}$$

which implies

$$\langle \mathbf{A}\mathbf{u}^1, \mathbf{u}^2 \rangle_E = \langle \mathbf{A}\mathbf{u}^2, \mathbf{u}^1 \rangle_E. \tag{19}$$

From equations (17) and (19) one obtains relation (15). This completes the proof of the theorem.

**VARIATIONAL THEOREM**

The necessary and sufficient condition that there exists a variational functional corresponding to the operator, equation (8), is that equation (19) holds for each  $\mathbf{u}^1, \mathbf{u}^2 \in E$ , i.e. the bilinear form must be symmetric in  $\mathbf{u}^1$  and  $\mathbf{u}^2$  [15].

The corresponding variational functional is given by

$$f(\mathbf{u}) = \frac{1}{2} \langle \mathbf{A}\mathbf{u}, \mathbf{u} \rangle_E + \langle \mathbf{f}, \mathbf{u} \rangle_E. \tag{20}$$

A demonstration of this important result can be found in ref. [16].

From equations (9)–(11), (13) and (20) (using Green's theorem and the property of the convolution) one obtains

$$f(\mathbf{u}) \equiv f(T, W) = \rho \int_B \left( \frac{1}{2} \delta c \left( \frac{\partial}{\partial t} (T * T) \right. \right.$$

$$\begin{aligned}
 & + \left. \left( a + \frac{\epsilon r a_m \delta}{c} \right) \nabla T * \nabla T + \epsilon r a_m \delta \nabla T * \nabla W \right. \\
 & + \left. \frac{1}{2} \epsilon r \left( \frac{\partial}{\partial t} (W * W) + a_m \nabla W * \nabla W \right) - \delta c T_0 T \right. \\
 & - \left. \epsilon r W_0 W \right) \Big) dV + \int_{\partial B_q} (\delta \hat{q} * T) dS + \int_{\partial B_j} (\epsilon r \hat{j} * W) dS \\
 & + \int_{\partial B_T} (\delta (T - \hat{T}) * q) dS + \int_{\partial B_w} (\epsilon r (W - \hat{W}) * j) dS.
 \end{aligned} \tag{21}$$

Thus,  $f(\mathbf{u})$  in equation (21) is the functional associated with  $\mathbf{A}\mathbf{u} + \mathbf{f}$  in equation (8); that is, the solution of the set of equations (1)–(7) is a critical point (a point  $\mathbf{u} \in E$  is called a critical point of the functional  $f(\mathbf{u})$  if  $\text{grad } f = \mathbf{0}$ ) of  $f$ . This is proved in the following theorem.

*Theorem 2.* Let  $\mathbf{u} \in E$ , and let  $f(\mathbf{u})$  have a linear Gâteaux differential at every  $\mathbf{u}$ , where  $f$  is the functional defined in equation (21). Then

$$\delta f(\mathbf{u}, \mathbf{u}') = 0 \tag{22}$$

if and only if  $\mathbf{u}$  is a solution of equation (8).

*Proof.* Let  $\mathbf{u}'$  be an arbitrary element in  $E$ . Then the Gâteaux differential of  $f$  is

$$\begin{aligned}
 \delta f(\mathbf{u}, \mathbf{u}') = & \langle \text{grad } f(\mathbf{u}), \mathbf{u}' \rangle_E = \rho \int_B \left( \delta c \left( \frac{\partial T}{\partial t} \right. \right. \\
 & - \left. \left. \left( a + \frac{\epsilon r a_m \delta}{c} \right) \Delta T - \frac{\epsilon r a_m}{c} \Delta W \right) * T' + \epsilon r \left( \frac{\partial W}{\partial t} \right. \right. \\
 & - \left. \left. a_m (\Delta W + \delta \Delta T) \right) * W' + \delta c (T(0) - T_0) T' \right. \\
 & + \left. \epsilon r (W(0) - W_0) W' \right) dV + \int_{\partial B_q} (\delta (\hat{q} - q) * T') dS \\
 & + \int_{\partial B_j} (\epsilon r (\hat{j} - j) * W') dS + \int_{\partial B_T} (\delta (T - \hat{T}) * q') dS \\
 & + \int_{\partial B_w} (\epsilon r (W - \hat{W}) * j') dS = \langle \mathbf{A}\mathbf{u} + \mathbf{f}, \mathbf{u}' \rangle_E.
 \end{aligned} \tag{23}$$

One first proves sufficiency. Suppose that  $\mathbf{u} \in E$  is a solution of equations (1)–(7). Then equation (23) becomes

$$\langle \mathbf{A}\mathbf{u} + \mathbf{f}, \mathbf{u}' \rangle_E = \langle \text{grad } f(\mathbf{u}), \mathbf{u}' \rangle_E = \mathbf{0} \tag{24}$$

which implies equation (22).

To prove the necessity, assume that equation (22) holds. In view of Lemmas 1–4 [17] one can see that

$$\text{grad } f(\mathbf{u}) = \mathbf{A}\mathbf{u} + \mathbf{f} = \mathbf{0}. \tag{25}$$

This completes the proof of the theorem.

## CONCLUSIONS

The results obtained in this paper can make a base to construct the numerical solutions of initial-boundary value problems of linear heat and mass transfer. The variational formulation for the finite element method [18] and the reciprocity equation for the boundary element method [19]. The fundamental solutions to this equation, corresponding to a concentrated heat and mass source, can be found in ref. [20].

## REFERENCES

1. A. V. Luikov, On thermal diffusion of moisture, *J. Appl. Chem.* **8**, 19–54 (1935) (in Russian).
2. A. V. Luikov, Moisture gradients in the drying clay, *Trans. Ceram. Soc.* **35**, 123–129 (1936).
3. A. V. Luikov, *Heat and Mass Transfer in Capillary-porous Bodies*. Pergamon Press, Oxford (1966).
4. A. V. Luikov and Y. A. Mikhailov, *Theory of Energy and Mass Transfers*. Pergamon Press, Oxford (1965).
5. A. V. Luikov, Systems of differential equations of heat and mass transfer in capillary-porous bodies (review), *Int. J. Heat Mass Transfer* **18**, 1–14 (1975).
6. O. Krischer, *Die Wissenschaftlichen Grundlagen der Trocknungstechnik*. Springer, Berlin (1963).
7. D. A. De Vries, Simultaneous transfer of heat and moisture in porous media, *Trans. Am. Geophys. Un.* **39**, 909–916 (1958).
8. I. J. Kumar, An extended variational formulation of the non-linear heat and mass transfer in a porous medium, *Int. J. Heat Mass Transfer* **14**, 1759–1770 (1971).
9. Yu. T. Glazunov, On the existence of the classic-type variational principle for non-linear interrelated heat and mass transfer, *J. Engng Phys.* **47**, 667–670 (1984) (in Russian).
10. Yu. T. Glazunov, Generalized variational principle of molar-molecular heat- and mass-transfer phenomena, *Int. J. Heat Mass Transfer* **23**, 759–763 (1980).
11. Yu. T. Glazunov, The variational method for the solution of the combined heat and mass transfer problems, *Int. J. Heat Mass Transfer* **26**, 1815–1822 (1983).
12. Yu. A. Mikhailov and Yu. T. Glazunov, *Variational Methods in the Theory of Non-linear Heat and Mass Transfer*. Izd. Zinatne, Riga (1985) (in Russian).
13. J. T. Oden and J. N. Reddy, *Variational Methods in Theoretical Mechanics*. Springer, Berlin (1976).
14. G. A. Korn and T. M. Korn, *Mathematical Handbook for Scientists and Engineers*. McGraw-Hill, New York (1968).
15. M. Kerner, Die Differentiale in der Allgemeinen Analysis, *Ann. Math.* **34**, 546–572 (1933).
16. M. M. Vainberg, *Variational Method for the Study of Nonlinear Operators*. Holden-Day, San Francisco (1964).
17. M. E. Gurtin, Variational principles for linear elastodynamics, *Archs Ration. Mech. Analysis* **16**, 34–50 (1964).
18. O. C. Zienkiewicz, *The Finite Element Method in Engineering Science*, 2nd Edn. McGraw-Hill, London (1971).
19. P. K. Banerjee and R. Butterfield, *Boundary Element Method in Engineering Science*. McGraw-Hill, London (1981).
20. J. Wyrwał, Boundary element method in the theory of heat and moisture transfer, submitted to *Arch. Thermodyn.* (1988) (in Polish).

## QUELQUES THEOREMES DANS LA THEORIE DE LUIKOV SUR LE TRANSFERT DE CHALEUR ET DE MASSE DANS LES CORPS MICROPOREUX

**Résumé**—On considère la théorie linéaire du transfert de chaleur et de masse. Quelques théorèmes généraux sont formulés tels que, par exemple, un théorème de réciprocity et un théorème variationnel (il n'est pas fait usage de la transformation de Laplace). La fonctionnelle utilisée donne toutes les équations fondamentales qui incluent les conditions aux limites et initiales, comme les équations d'Euler.

## EINIGE THEOREME ZUR LUIKOV'SCHEN THEORIE DES WÄRME- UND STOFFTRANSPORTS IN KAPILLAR-PORÖSEN KÖRPERN

**Zusammenfassung**—Die lineare Theorie des Wärme- und Stofftransports wird betrachtet. Einige allgemeingültige Theoreme werden formuliert, z. B. ein Reziprozitätstheorem und ein Variationstheorem (die Laplace-Transformation wird nicht verwendet). Das hier hergeleitete Funktional ergibt alle maßgebenden Gleichungen sowie die Rand- und Anfangsbedingungen und die Euler-Gleichungen.

## НЕСКОЛЬКО ТЕОРЕМ ТЕОРИИ ТЕПЛО- И МАССОПЕРЕНОСА ЛЫКОВА В КАПИЛЛЯРНО-ПОРИСТЫХ ТЕЛАХ

**Аннотация**—Рассматривается линейная теория тепло- и массопереноса. Сформулировано несколько общих теорем, а именно, теорема взаимности и вариационная теорема (без использования преобразования Лапласа). Выведенный функционал дает возможность получить все основные уравнения типа уравнений Эйлера с граничными и начальными условиями.